PUMP TEST REPORT PROPOSED TAUNTON PUMP STATION

Proposed Taunton Pump Station Project 690 West Water Street Taunton, Massachusetts

Prepared for:

BETA Group, Inc. 6 Blackstone Valley Place Lincoln, RI 02865

Prepared by:

Paul B. Aldinger & Associates, Inc. 860A Waterman Avenue, Suite 9 East Providence, Rhode Island 02914

> PBA No. 17006 June 2018

June 1, 2018

Mr. Christopher Cronin, P.E. Project Manager BETA Group, Inc. 6 Blackstone Valley Place Lincoln, RI 02865

Re: Pump Test Report Proposed Taunton Pump Station 690 West Water Street Taunton, Massachusetts PBA Job No. 17006

Dear Mr. Cronin:

Paul B. Aldinger & Associates Inc. (PBA) is pleased to provide BETA Group Inc. (BETA) with this geotechnical engineering report for the above referenced project. This report is subject to the limitations that are outlined in Appendix A.

1.00 INTRODUCTION, PROJECT DESCRIPTION, AND PUMP TEST WORK SCOPE OBJECTIVES

The project consists of constructing a new Main Sewage Pump Station, and influent sewage pipeline with intermediate manhole structures located north and west of the proposed pump station, beneath West Water Street in Taunton, Massachusetts. Additionally, two "twin" 24 inch diameter sewer force mains are planned to extend south from the proposed pump station to the Taunton Waste Water Treatment Plant. The proposed pump station is planned to be located directly adjacent and east of the existing pump station, at 690 West Water Street, Taunton, Massachusetts. Refer to the attached Figure 1, Site Vicinity Plan.

For project background information refer to the following:

- <u>Geotechnical Engineering Report</u> for the Proposed Pump Station and Stream Crossing, Taunton, Massachusetts; Paul B. Aldinger and Associates; August 16, 2017.
- <u>Main Lift Pump Station Drawings</u>, City of Taunton, Massachusetts; BETA Group Inc., April 2018.

• <u>Existing Pump Station, Test Pit Report</u>; Paul B. Aldinger and Associates; June 1, 2018

The proposed pump station will be located less than approximately 10 feet to the east of the existing pump station, and will be founded deeper than the existing pump station. The results of a recent test pit program undertaken adjacent to and along the east and west perimeter foundation walls of the existing pump station indicated no sheet piling exists around and below the existing pump station's foundation. This absence of sheeting potentially makes the existing pump station sensitive to the proposed adjacent deep construction.

Due to the proximity of the two pump station structures, the existing shallow groundwater depth, and the depth of proposed pump station construction, support-of-excavation and construction dewatering systems will be required for the new construction, particularly considering that the proposed pump station foundation will extend below the existing pump station foundation.

The site for the proposed pump station is presently asphalt paved and relatively flat with an existing ground surface elevation of approximately +11.5 feet. According to the project drawings, the existing station's mat foundation bottom is at elevation -19.7 feet, approximately 31 feet below ground surface. The proposed pump station will be founded with the top-of-mat foundation at elevation -21.5 feet. The structure's mat foundation is anticipated to be on-the-order of 3 to 5 feet in thickness, which would place a 5 foot thick mat bottom at the approximate elevation of -26.5 feet, 38 feet below the ground surface.

Other significant project facets include:

- To the east of the proposed pump station, the site slopes downward to the Taunton River. There is an existing sewer siphon extending from beneath the Taunton River into the existing pump station that currently bisects the proposed pump station foot print. The sewer siphon pipeline will need to be integrated into the proposed pump station.
- An extensive and deep system of influent sewer pipeline and manhole structures are planned to be constructed below West Water Street, leading to and supplying the proposed pump station.
- Two "twin" 24 inch diameter sewer force mains are planned to exit the proposed pump station on the south side, and extend south approximately one-quarter (¼) mile, with one stream crossing, to the Taunton Waste Water Treatment Plant located at 825 West Water Street.

This report focuses on the procedures, performance data and analysis results of a groundwater

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Pump Test program undertaken to develop design-phase hydraulic data for the proposed pump station's support-of-excavation and construction dewatering designs, which are linked. The proposed pump station's excavation is estimated to extend approximately 40 feet below ground surface.

The Pump Test was performed from a pump well located within the footprint of the proposed pump station during March of 2018. The construction dewatering approach for the proposed pump station is recommended to consist of the dewatering of the varved SILT stratum (Glacial Outwash 1), which extends approximately to the bottom of the proposed pump station excavation, and the dewatering/depressurization of the coarse granular stratum described as fine to coarse SAND and to trace gravel (Glacial Outwash 2) located between approximately 40 and 68 feet below ground surface. The fine to coarse SAND and to trace Gravel stratum was the focus of the Pump Test program. The strata identification terms Glacial Outwash 1 and Glacial Outwash 2 are from the project's Geotechnical Report.

The project's elevation datum is the North American Vertical Datum of 1988 (NAVD 88), and the horizontal datum is North American Datum of 1983 (NAD 83).

Work scope objectives of the Pump Test are to:

- Provide data for the successful Contractor to develop an estimated range of permeability values (k value range) for the proposed pump station's construction dewatering design. The construction dewatering effort will focus on the dewatering of the varved SILT stratum (Glacial Outwash 1) and the depressurization/dewatering of the coarse granular stratum (Glacial Outwash 2) located approximately 40 to 68 feet below existing ground surface.
- Provide data for the successful Contractor to develop an estimated range of construction dewatering pump rate (steady-state) and an estimated areal extent of construction dewatering influence zone (groundwater level zone of depression), based upon the depth of proposed pump station support-of-excavation system, i.e. based upon the extent of coarse granular stratum groundwater cut-off by the proposed sheet pile system. The anticipated support-of-excavation system is a braced steel sheet pile system approach to support an excavation depth of approximately 40 feet below ground surface.

2.00 CHRONOLOGY OF SIGNIFICANT PROJECT EVENTS

• Project <u>Boring Program Performance</u>, PBA-1 through PBA-5: February 27 to March 3, 2017.

- Project <u>Geotechnical Report</u> submission: August 16, 2017.
- <u>Existing Pump Station, Test Pit Program</u>:, October 27, 2017.
- <u>Pump Well and Pump Installation</u>:, January 9 to January 11, 2018.
- <u>Existing Pump Station, Vertical Movement Monitoring Point Installations</u>: February 2 to February 28, 2018.
- Pump Test <u>Monitor Well Installations</u>, MW-1, 2 and 3: February 5 to February 22, 2018.
- <u>Pump Well, Step Test Performance</u>: Morning of March 19, 2018.
- <u>Pump Test Performance</u>: Afternoon of March 19 to March 22, 2018.
- <u>Pump Test Equipment Demobilization</u>: March 23, 2018.
- Existing Pump Station, Vertical Movement Monitoring Point Elevation Checks: March 23, 2018.
- <u>Pump Test Data-Logger Demobilization</u>: March 29, 2018.

3.00 PROPOSED PUMP STATION AREA, SUBSURFACE STRATIGRAPHY

For the following discussion refer to:

- Figure 2, Pump Station Area Locations: Borings, Pump and Monitor Wells.
- Figure 3A, Pump Station Area Locations: Subsurface Profile A-A and Schematic Profile B-B.
- Figure 3B, Pump Station Area: Subsurface Profile A-A.
- Appendix B: Boring Logs PBA-1 and PBA-2; and Grainsize Analysis Pump Well Screen Stratum: Soil sample from boring PBA-1, Glacial Outwash 2 stratum (F/C SAND and/trace Gravel stratum) sample depth 49 to 56 feet below ground surface.

A brief description of the subsurface stratigraphy encountered within and surrounding the proposed pump station foot print, utilizing project borings PBA-1 and PBA-2 and Geotechnical Report terminology, is described from top to bottom:

• <u>Existing Ground Surface</u>, elevation +11.5.

- <u>Granular Non-Engineered Fill</u> extending to between approximately 17 and 20 feet below ground surface (elev. -5.5 to -8.5). This stratum is generally described as: variably loose to dense; brown/gray; mixture of Sand, Gravel and Silt with wood encountered at bottom-of-stratum in boring PBA-1.
- <u>Glacial Outwash 1</u> extending to between approximately 30 and 40 feet below ground surface (elev. -18.5 to -28.5). This granular stratum is generally described as: medium dense; gray; varved inorganic SILT (ML).
- <u>Glacial Outwash 2</u> extending to approximately 68 feet below ground surface (elev. -56.5). This granular stratum is generally described as: medium dense to very dense; gray; fine to coarse SAND, and to trace Gravel, trace Silt (SP-SM). This stratum is the focus of the Pump Test and the location of the Pump Well screen. Note: the pump well installation log indicates the presence of cobble size rock components within this stratum.
- <u>Glacial Till</u> extending to approximately 72 feet below ground surface (elev. -60.5). This granular stratum is generally described as: very dense; gray; fine to coarse SAND AND GRAVEL, trace Silt (SP-SM).
- <u>Bedrock</u> (assumed, not core sampled) with approximate surface at 72 feet below ground surface (elev. -60.5). From the literature, area bedrock is the relatively soft Rhode Island Formation composed typically of interbedded Shale, Sandstone and/or Conglomerate rock types.
- <u>Groundwater Level</u>: From the groundwater monitoring well installed within borehole PBA-1: on March 3, 2017 groundwater level was approximately 7.2 feet below ground surface (elev. +4.3); and on March 19, 2018 groundwater level was approximately 5.0 feet below ground surface (elev. +6.5).

4.00 PUMP TEST PROGRAM COMPONENTS

For the following Report Section 4.00 discussion, refer to:

Appendix C: J. Russell Water Well Inc. Information Package:

- Step and Pump Tests, Pump Well Summary Data.
- Submersible Pump, Grundfos model 300S100-3A, Pump Performance Curves.
- Step Test Data, Pump Well: Pump Rate, Pump Well Groundwater Level, Time.

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- Pump Test Data, Pump Well: Pump Rate, Pump Well and Boring PBA-1 Monitoring Well Groundwater Level, Time.
- Pump Well and Well Screen Installation Log.

Components of the Pump Test program include:

- Pump well and submersible pump installations.
- Monitor and pump wells, vibrating-wire piezometer installations.
- Existing pump station, vertical movement monitoring point installations.
- Pump well, Step Test performance.
- Pump well, Pump Test performance.

4.10 PUMP WELL AND SUBMERSIBLE PUMP INSTALLATIONS

Between Tuesday January 9 and Thursday January 11, 2018, the Viera Well Company of Georgetown, Massachusetts in coordination with J. Russell Water Well Inc. of Hope Valley, Rhode Island installed and logged the pump well casing/screen, and set the submersible pump. Well construction consisted of standard 8 inch I.D. steel casing extending to 50 feet below ground surface, with an 8 inch I.D. by 10 foot long, 50 slot, stainless steel well screen without filter pack set below the casing, between depths of 50 and 60 feet below ground surface. The well screen was set at the approximate middle of the coarser granular stratum (Glacial Outwash 2), herein after referred to as the "aquifer stratum". Well drilling procedures consisted of air-rotary drilling between 47 and 65 feet. Water-rotary drilling procedures were used within the aquifer stratum and well screen depth zone to limit stratum contamination by the mud-rotary drilling procedure.

The Pump Test's submersible pump was set within the well casing at an intake depth of 43 feet below ground surface. The pump was a 10 hp Grunfos model 300S100-3A submersible 3-stage turbine pump, capable of pumping a maximum of 400 gallons per minute (gpm) against a water head of 50 feet. Power for the pump testing was obtained from the existing pump station's electrical panel. Also installed within the pump well casing was facility for the well driller to monitor groundwater level before, during and after pump testing. In-well hand measurement of groundwater level was performed by the well driller periodically using a Solonist electronic water level meter, as a back-up to an in-well vented vibrating-wire piezometer installed by PBA.

Pump Test discharge was conveyed to the existing pump station's wet well through approximately 45 feet of 6 inch I.D. PVC pipe installed between the well head and wet well through an opening cut-into a (temporary) securely bolted plywood cover over an existing pump station exterior wet well access-way. Pump Test discharge flow volume was measured by an in-line PVC pipe digital flow meter installed approximately mid-way between the well head and wet well discharge point.

4.20 MONITOR AND PUMP WELLS, VIBRATING-WIRE PIEZOMETER PROGRAM

For the following discussion refer to Figure 2, Pump Station Area Locations: Borings, Pump and Monitor Wells; Figure 3A, Pump Station Area Locations: Subsurface Profile A-A and Schematic Profile B-B; and Figure 4, Pump Station Area, Schematic Subsurface Profile B-B: Borings, Pump and Monitor Wells.

Between Monday February 5 and Thursday February 22, 2018, New England Boring Contractors of Derry, New Hampshire installed three (3) groundwater monitoring wells at locations selected by PBA. Monitor well installations were observed and guided by a PBA geotechnical engineer and/or engineering technician. Monitor wells were located at specific distances from the pump well for analysis purposes: MW-1 at approximately 5 feet, MW-2 at approximately 50 feet, and MW-3 at approximately 100 feet. Each monitor well was constructed to contain three (3) vibrating-wire piezometers (Geokon 4500S-700KPA, unvented) located at borehole depths for stratum specific groundwater level information. Vibrating-wire piezometers were installed by first advancing and cleaning nominal 4 inch diameter steel casing (HW) by the drive and wash method to several feet below the deepest piezometer depth. At ground surface, the three (3) piezometers and their wiring were attached to a nominal 1 inch diameter PVC pipe at specific depth intervals, which was then lowered to bottom-of-casing at borehole center. The PVC pipe was now used as a tremie pipe to cement-bentonite grout the borehole orifice with piezometers in-place, from borehole bottom to ground surface while extracting the four (4) inch diameter casing.

Additionally, a "vented" barometric pressure compensating vibrating-wire piezometer (Geokon 4500SV-700KPA, vented) was installed within the pump well at a groundwater depth deep enough to not be impacted by Pump Test draw-down, at a depth below ground surface of approximately 46 feet.

Each monitor well piezometer was located at the approximate center of the three (3) principal saturated soil strata, from top to bottom: the granular non-engineered Fill, varved SILT (Glacial Outwash 1) and coarse granular stratum(Glacial Outwash 2) as seen in the pump station area boring logs PBA-1 and PBA-2. Vibrating-wire piezometers were set at the following approximate depths below ground surface in each of the three (3) monitor wells, from top to bottom: 9 feet, 28 feet and 55 feet. Within MW-1, located approximately 5 feet from the pump well, the bottom piezometer was set at the adjacent mid-pump well screen depth, coincidentally at 55 feet below ground surface, to record immediate well adjacent groundwater level during the Step and Pump testing.

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All nine (9) monitor well and the one (1) pump well piezometers were wire connected to a 16 channel data logger (Geokon 8002-16-2; LC-2x16) for simultaneous groundwater data collection during the Step and Pump Testing. There are two types of vibrating-wire piezometers, those that are open to the atmosphere or "vented" and those that are not. Vented piezometers are designed to apply a barometric pressure compensation to readings, unvented (hermetically sealed) piezometers do not.

For piezometer applications within groundwater regimes not open to the atmosphere, e.g. most below ground surface applications and within grouted boreholes, the full effects of barometric pressure may be attenuated, delayed or otherwise minimized. In this case, the application of barometric pressure compensation to groundwater level readings may introduce significant errors. For example, a barometric pressure change from 29 to 31 inches of mercury would result in approximately one (1) psi of barometric pressure reading correction or up to 2.3 feet of groundwater level error. For this application, an unvented (or sealed) piezometer would be appropriate, e.g. the nine (9) unvented piezometers installed in the project's groundwater monitor wells MW-1, 2 and 3.

For piezometer applications where the water column is open to the atmosphere, e.g. within and open borehole or well, a vented or barometrically compensated piezometer will more accurately reflect groundwater pressure and thus groundwater level conditions. Piezometer venting is typically obtained through a dedicated vented signal cable, e.g. the vented piezometer installed in the project's pump well.

4.30 EXISTING PUMP STATION, VERTICAL MOVEMENT MONITORING POINT PROGRAM

For the following discussion refer to Figure 5, Existing Pump Station, Vertical Movement Monitoring Point Locations; and Appendix D: Surveyor's Sketch, Existing Pump Station Vertical Movement Monitoring Point Locations, and Monitoring Point Spreadsheet Data; and Main Lift Pumping Station, Taunton, MA, "Vertical Control (Locations)," Figure 1, BETA Group Inc.

Vertical movement monitoring points were installed on the existing pump station structure to record and document any structure movement that could be associated with the Pump Test program.

Bench mark, vertical survey control points were obtained from locations outside of the immediate pump station area on West Water Street, and control point elevations were brought onto the pump station site to verify known bench mark elevations on and around the existing pump station structure. A total of twelve (12) existing pump station perimeter, interior and exterior, vertical movement monitoring points were installed, and elevations obtained and checked, prior to the Pump Test performance. Vertical movement monitoring point elevations

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were determined to level survey accuracy, $1/100^{th}$ of a foot, $\pm 1/8^{th}$ inch. Post Pump Test performance, all structure vertical movement monitoring points were checked for elevation variation. To level survey accuracy, <u>no</u> vertical movement was detected at any of the monitoring points.

4.40 STEP TEST PROCEDURE AND WELL DRILLER PUMP WELL DATA SUMMARY

On the morning of Monday, March 19, 2018 the pump well was Step Tested to develop a sustainable pumping rate for the immediately following three (3) day Pump Test. Step Testing involves the sequential pumping of a well over a relatively short time period, in increasing pump rate increments, to determine a maximum safe pumping rate for the subsequent extended period Pump Test. During Step Test pumping, pump and monitor well groundwater level measurements are made to determine a pumping rate that provides drawn-down groundwater levels within the pump well that do not jeopardize pump function, and provides a pumping rate sufficient to induce a suitable groundwater level (aquifer) reaction to ultimately estimate aquifer hydraulic properties from the Pump Test results.

Prior to Step Test start, static groundwater level within the pump well was measured to be approximately 5.3 feet below ground surface, elev. +6.1. The first step pumping rate was 100 gpm, which produced an in-well groundwater level of 21.1 feet below ground surface. The second step pumping rate was 150 gpm, which produced an in-well groundwater level of 25.2 feet below ground surface. The third step pumping rate was 200 gpm, which produced an in-well groundwater level of 32.1 feet below ground surface. The groundwater level, 32.1 feet below ground surface, leaves a safety factor of approximately 11 feet of water above the submersible pump's intake, which was set at 43 feet below ground surface. After review of monitor well piezometer data, it was decided that a Pump Test pumping rate of 200 gpm would be appropriate and adequate.

At Step Test completion, groundwater conditions at the pump well recovered to within 0.34 feet (4 inches) of initial static conditions within approximately one (1) hour. At that time, the three (3) day Pump Test was initiated.

4.50 PUMP TEST PROCEDURE AND WELL DRILLER PUMP WELL DATA SUMMARY

On the afternoon of Monday, March 19, 2018 the three (3) day Pump Test was initiated. A constant pumping rate of 200 gpm was maintained until test completion on the afternoon of Thursday March 22, 2018. The maximum depth of in-well groundwater level was recorded to be 35.7 feet below ground surface. The in-well groundwater level recovered to 1.8 feet below static level within 30 minutes after pumping termination.

At the end of the Pump Test program the submersible pump was removed and the pump well screen/casing was left-in-place and capped with a bolted steel plate. Top of pump well capped casing is approximately 1.9 feet above ground surface.

5.00 SUMMARY: MONITOR AND PUMP WELLS VIBRATING-WIRE PIEZOMETER DATA

Prior to initiating the pump test the vibrating wire piezometers were installed and connected to the data logger. The piezometers were preset to record pressure readings at predetermined intervals. The results of these pressure readings were later downloaded and these readings used to develop the drawdown at each location by subtracting from the initial readings. These drawdown readings were then used to develop several plots which present the reaction of the groundwater at the piezometer level to the stress caused by the pumping of the well. See Appendix C for a summary of the well and observation well data.

Figures 6 through 8 present the drawdown measured in each of the piezometers as a result of the pumping of the well measured at each level versus the time since the start of the pump test. We note that the "top" piezometer was set 9 feet below ground surface, the "Mid" piezometer was set 28 feet below ground surface and the "Btm" piezometer was set 55 feet below ground surface in each piezometer. It is noted that most locations do indicate a tidal effect, and as expected the most drawdown is observed in the lowest piezometer at each location (btm) which was set in the sand and gravel stratum which was being pumped. The other piezometers are set in the varved silt (mid) and the granular fill (top) which show a significant retarding of the drawdown effect. This indicates that there is not good communication between these upper strata and the sand and gravel stratum which is being pumped.

Figures 9 through 11 present the drawdown measured in each of the piezometers within the same stratum (at the same depth) as a result of the pumping of the well. Figure 9 presents the drawdown in the fill layer measured in each piezometer set in that layer (at the same depth). We note here that the piezometer in MW-2 appears to be affected by the tidal influence more than the others and this retards the drawdown observed. The retardation of drawdown with distance from the pumping well is not entirely evident since the piezometer in MW-2 (50 feet from the pumping well) appears to have less drawdown than the one in MW-3 (100 feet from the pumping well), presumably due to tidal impacts. Figure 10 presents the drawdown in the varved silt stratum (mid Piezometer) measured in each piezometer set in that stratum (at the same depth). We note here that all of the piezometers appear to be affected by the tidal influence but the one in MW-2 appears to be affected more than the others. The retardation of drawdown with distance from the pumping well is more evident in this stratum.

Figure 11 presents the drawdown in the coarser stratum ("btm" Piezometer) beneath the varved silt measured in each piezometer set in that stratum (at the same depth). We note that the piezometer in MW-2 does not react as quickly as the other two, presumably due to tidal effects.

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We also note the effect of a reduction in drawdown with distance from the pumping well in the stratum.

For comparison, Figure 12 presents the results of all nine piezometers on the same plot. This clearly depicts the retardation of drawdown in the upper two strata, the fill (in blue) and the varved silt (in red). The fill layer sees very little effect and the varved silt is reduced by more than 50%. This demonstrates the lack of a good hydraulic communication among the strata. We can observe the retardation of drawdown with distance from the pumping well as well.

Figure 13 presents the drawdown in the three piezometers which are all in the coarser sand and gravel stratum beneath the varved silt versus the time since the initiation of the pump test. This figure presents the same information as in Figure 11 but adds the measurement of the drawdown in the pumping well. This clearly depicts the retardation of drawdown with distance from the pumping well.

Figure 14 presents the drawdown in the three piezometers ("btm" Piezometers)which were measured at the end of the pumping test. Also indicated are the hand measurements of drawdown in observation well PBA-1 which was screened in this stratum as well. Figure 15 presents the same information but adds the measurement of the drawdown in the pumping well. We believe that the break in the line from the piezometer at five feet to the pumping well is due to the inefficiency of this well.

6.00 ANALYSIS AND CONCLUSIONS

The excavation for the construction of the proposed new pump station will require the driving of sheeting to limit the extent of the excavation and protect nearby structures and ancillary development. This sheeting may also be utilized to limit the extent and type of dewatering required to stabilize the excavation. The soil at the bottom of the excavation (most likely the varved silt) must be dewatered, however due to the nature of the soil profile, the sand and gravel stratum beneath the excavation will also have to be depressurized. The results of this pumping test provides actual distance drawdown and hydraulic conductivity data for this underlying sand and gravel stratum as well as information on the hydraulic communication among the identified strata. We utilized this data along with our estimate of the thickness of this sand and gravel stratum in which the pump was set to estimate the hydraulic conductivity of this stratum at 5.4×10^{-2} cm/sec.

This data must be utilized by the successful contractor for the project to design the dewatering system to dewater the excavation for the pump station and to depressurize the underlying sand and gravel stratum. It will also be utilized to determine the depth which the sheeting will be driven to assist in the dewatering operation, perhaps driving the sheeting deeper than is required for structural stability, thus effecting a partial or full cutoff by driving the sheeting into the underlying glacial till deposit. This data will also be very helpful in designing the dewatering system required

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west of the proposed pump station, beneath West Water Street.

We appreciate to have been of service to you and we trust the information contained in this report is adequate for your needs at this time. Please contact the undersigned if there are questions on these recommendations or if you need additional information.

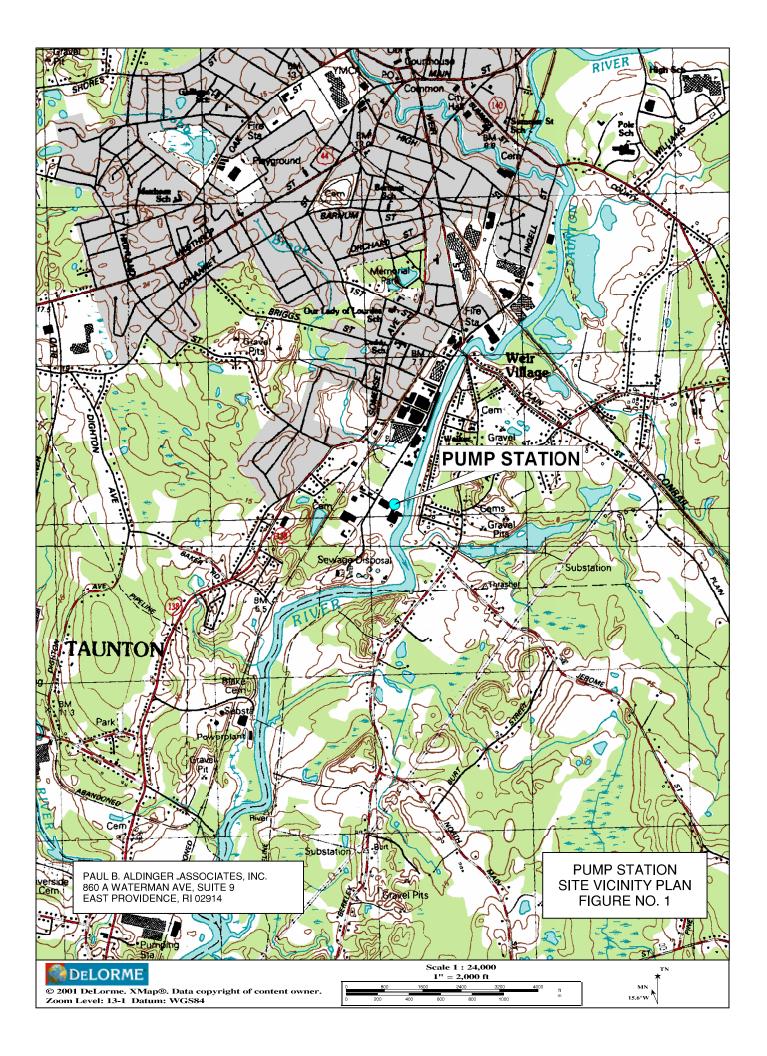
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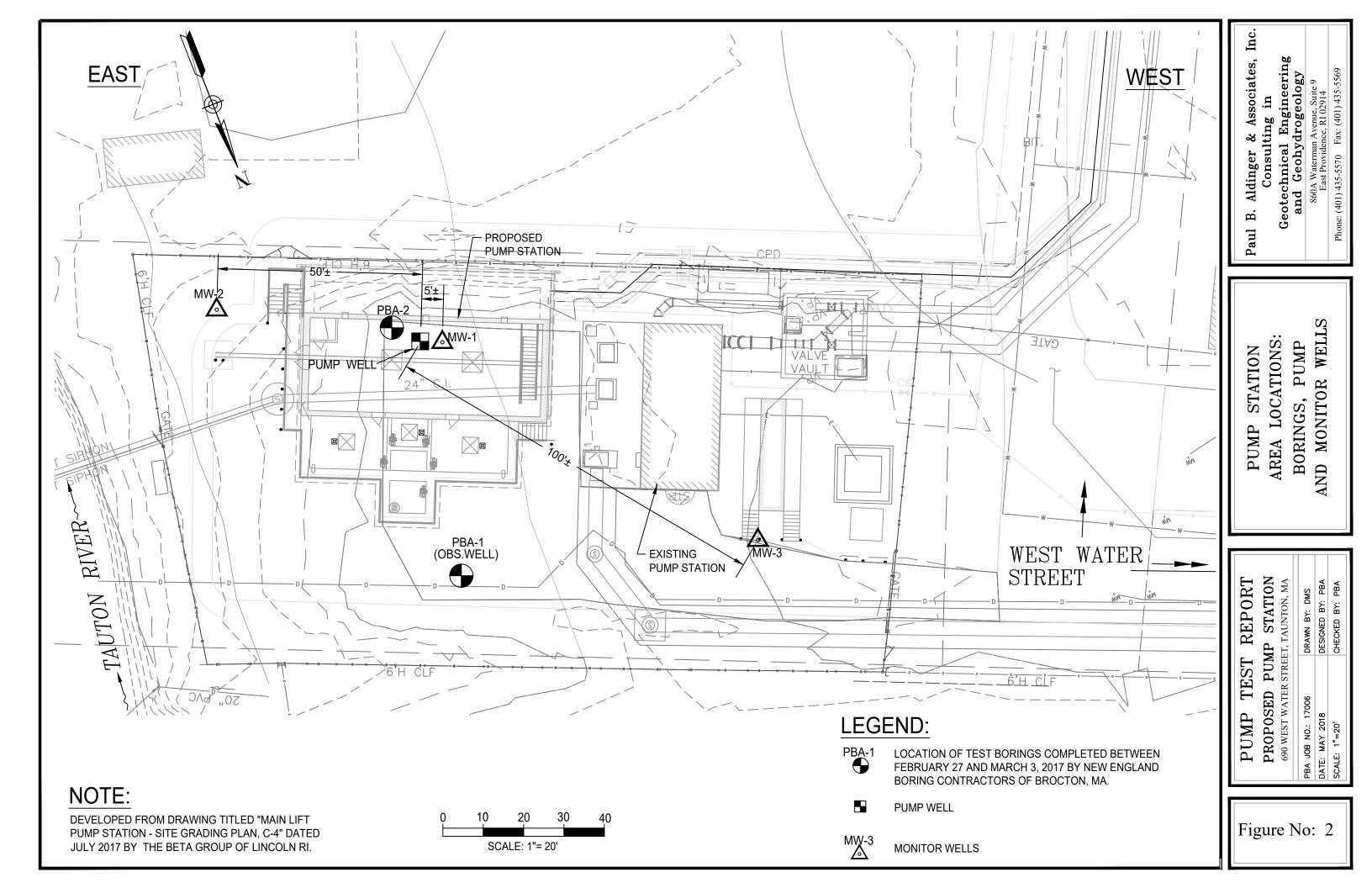
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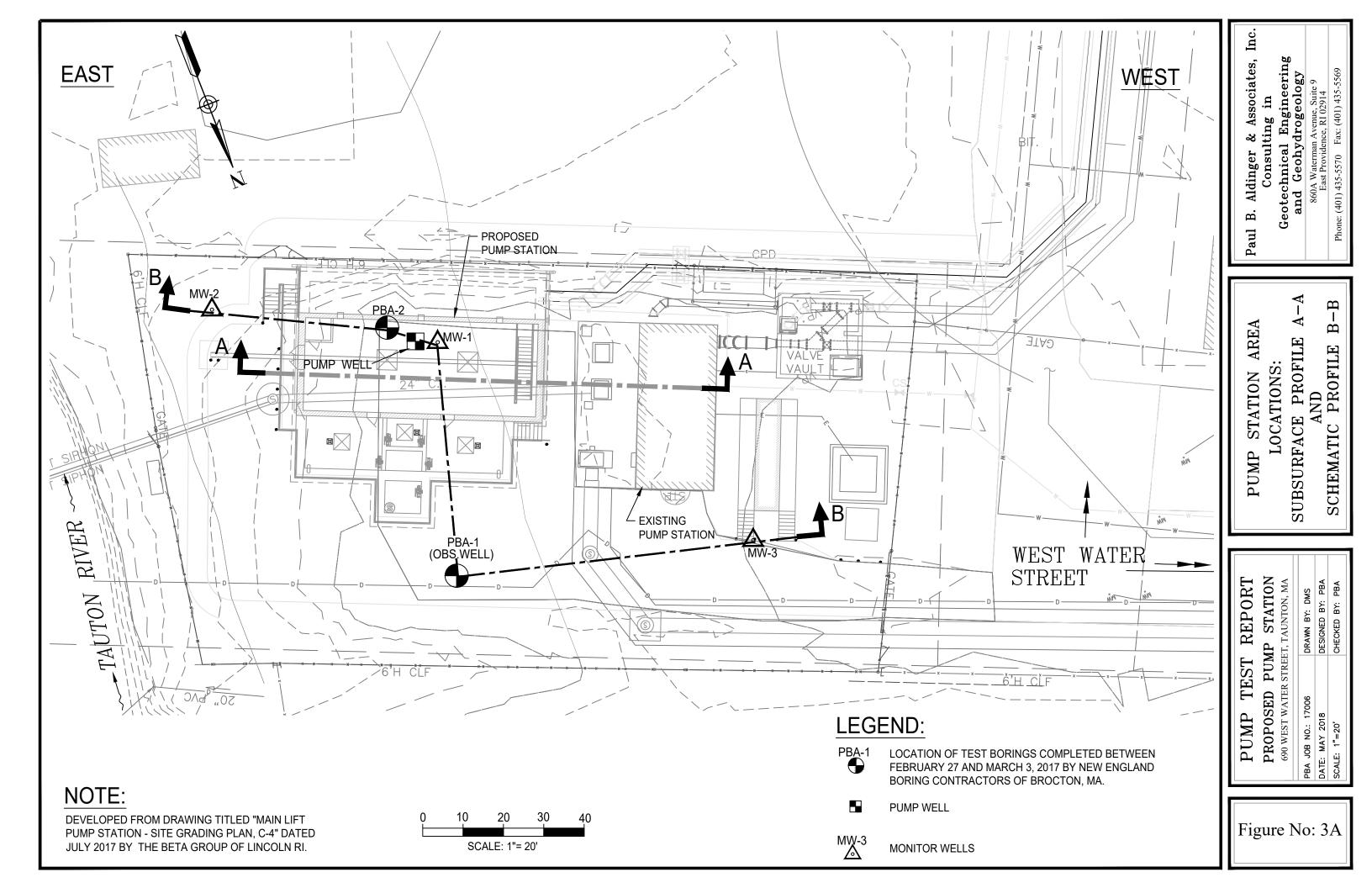
Paul B. Aldinger, Ph.D., P.E. Chief Engineer

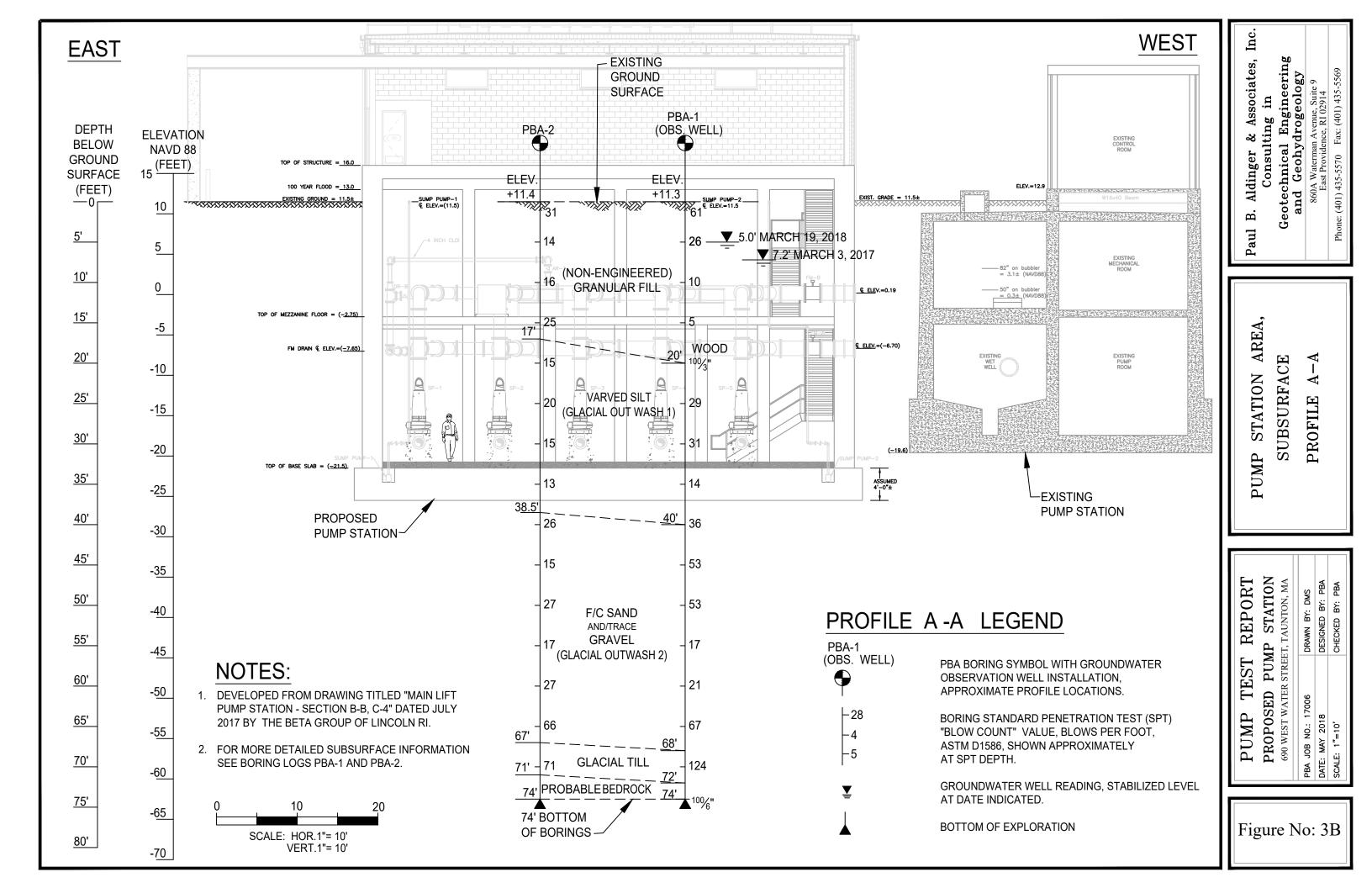


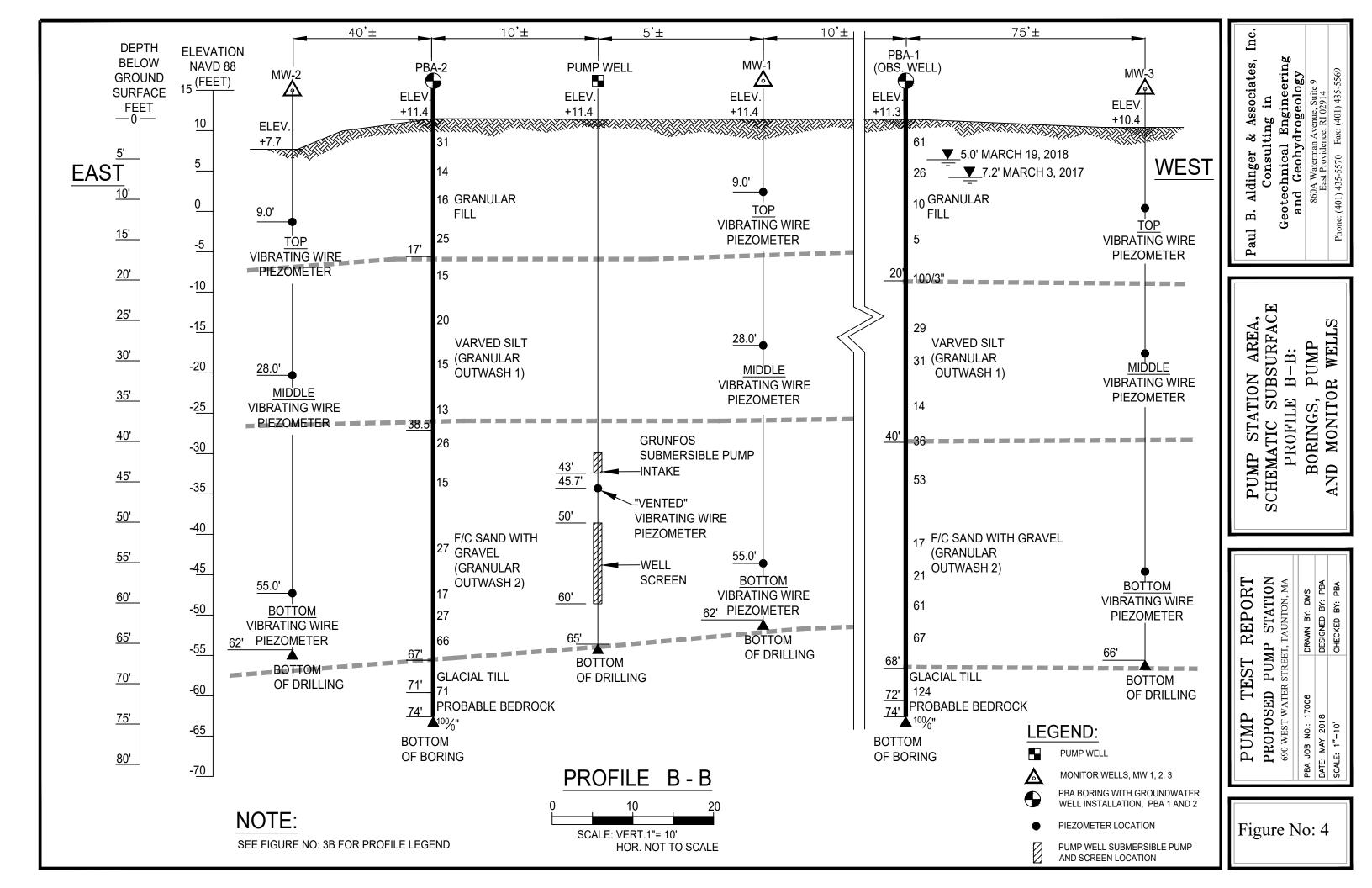
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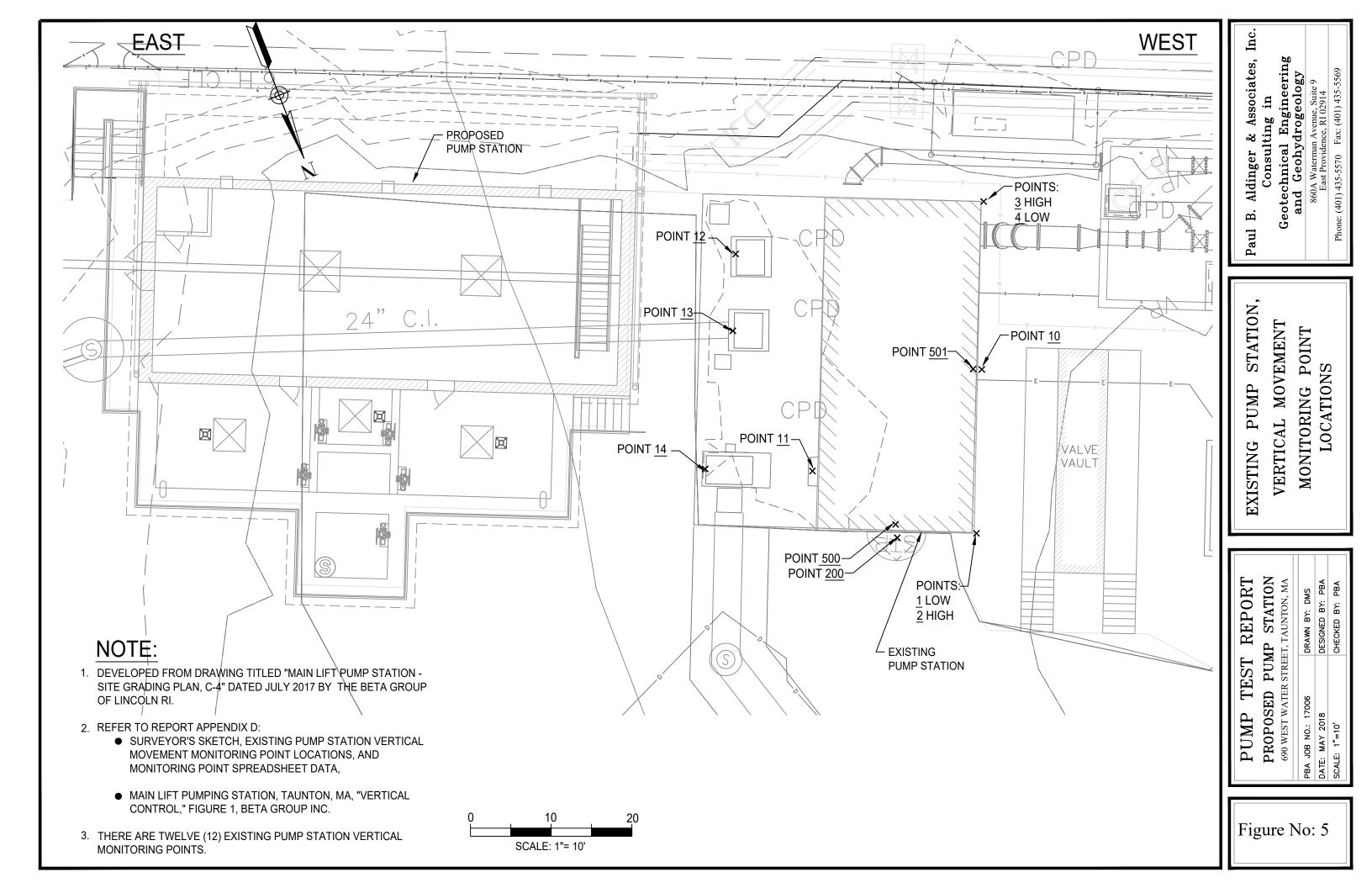


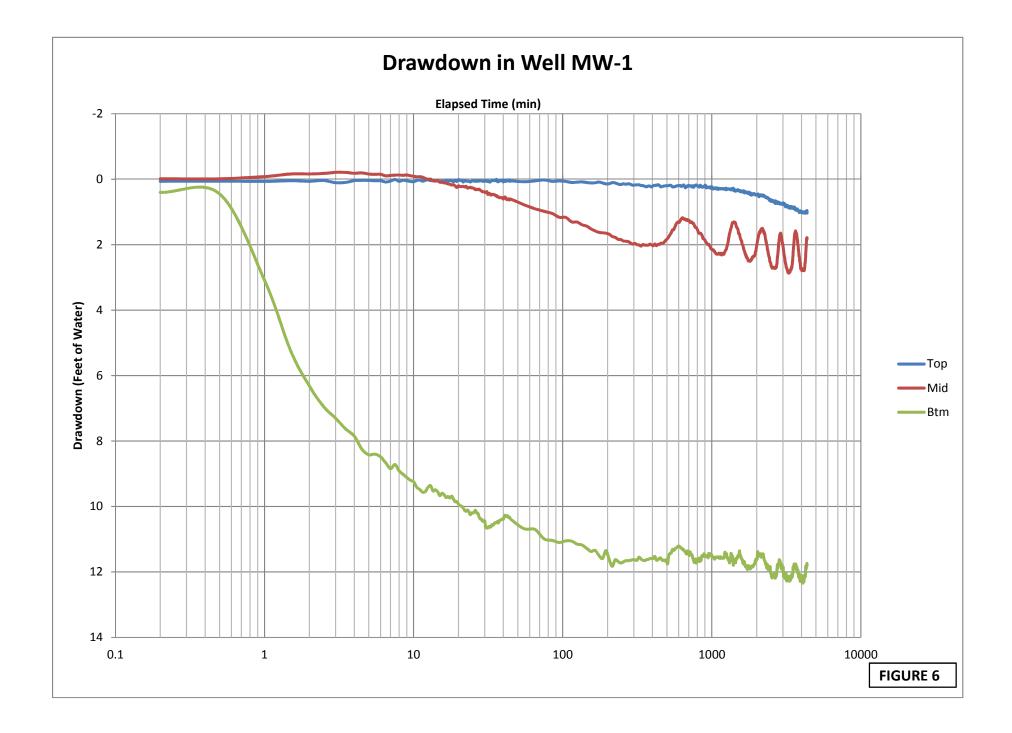


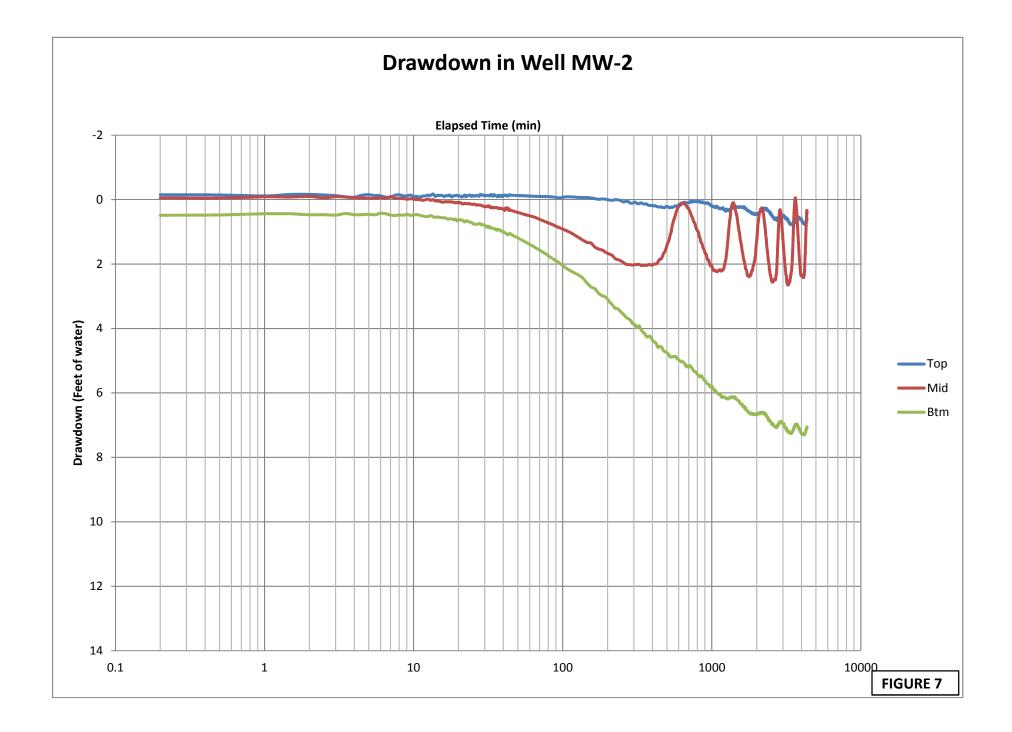


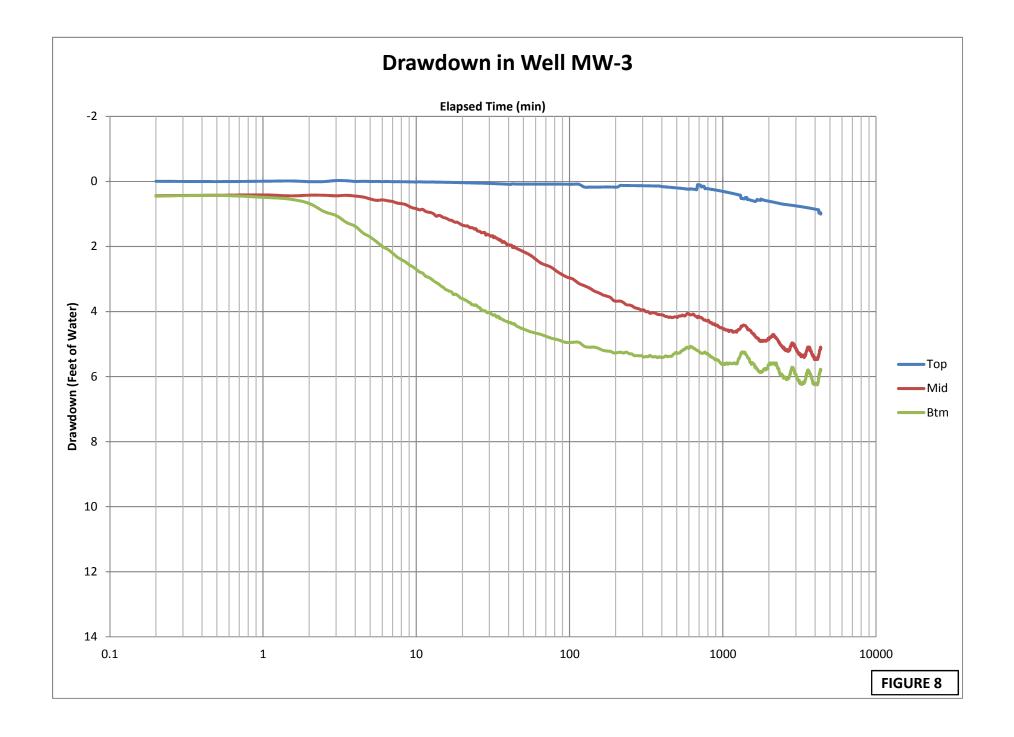


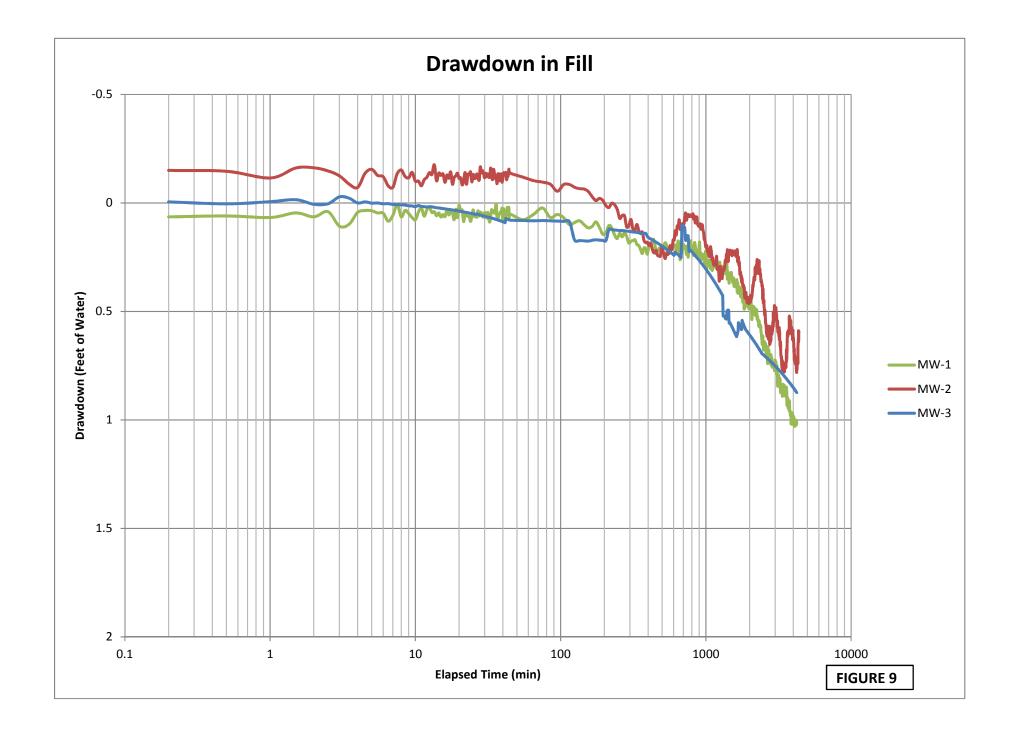


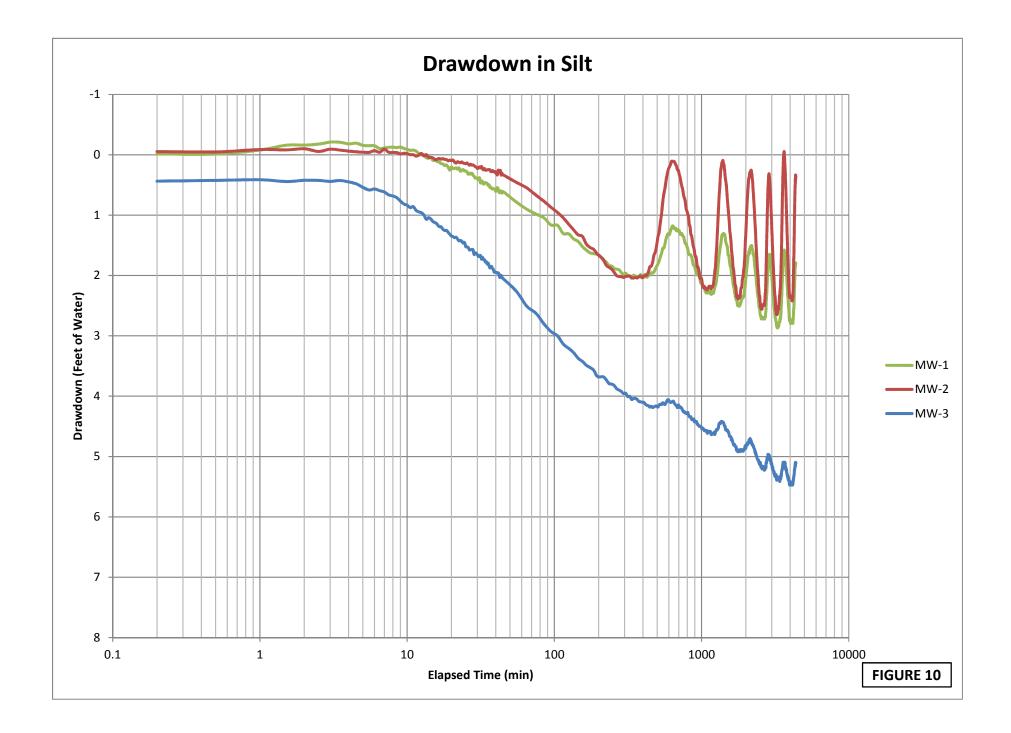


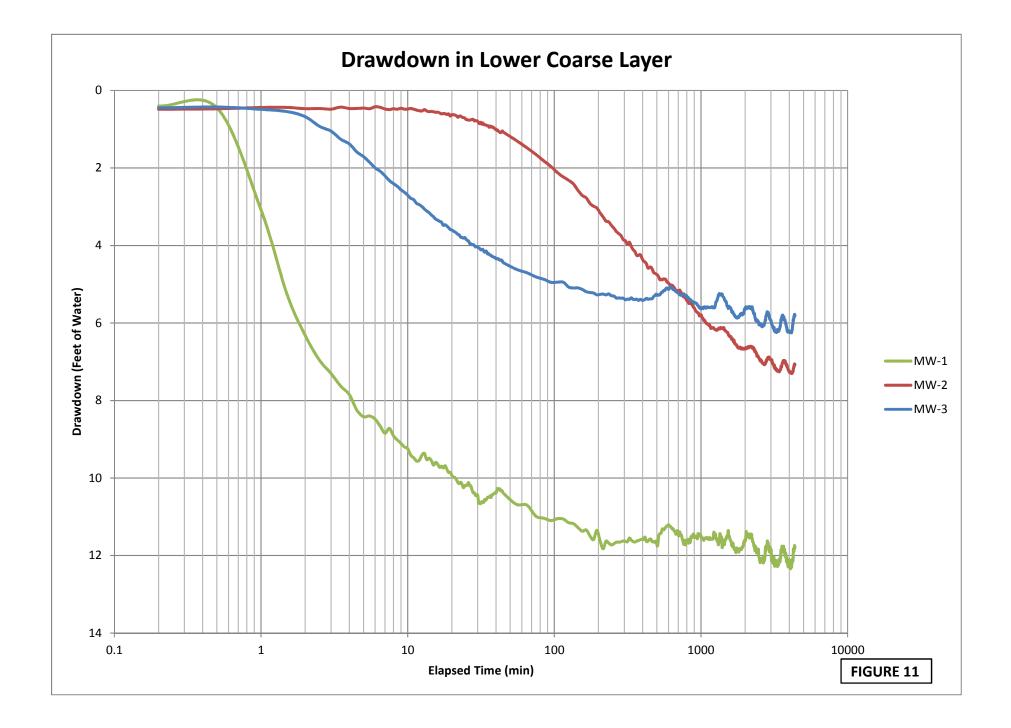


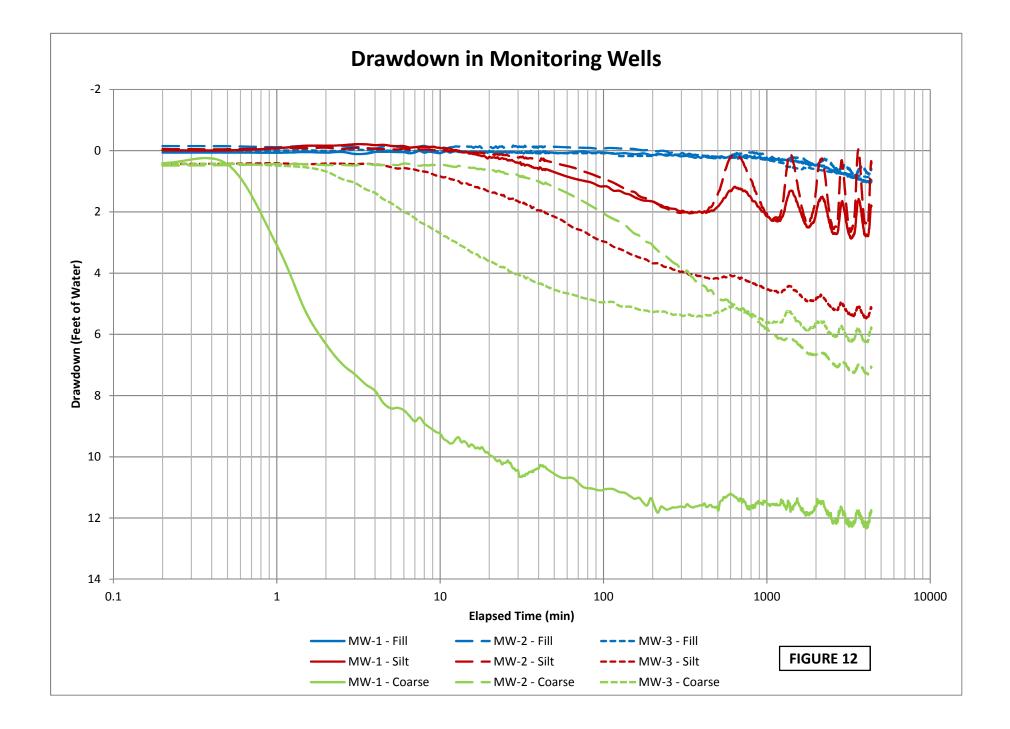


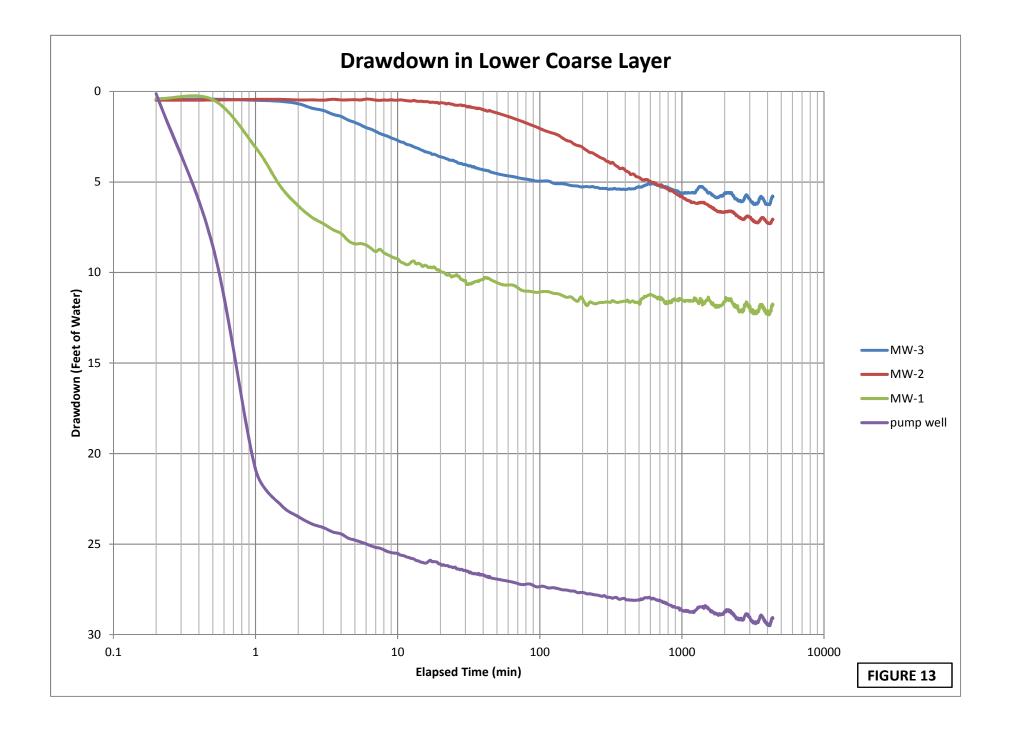


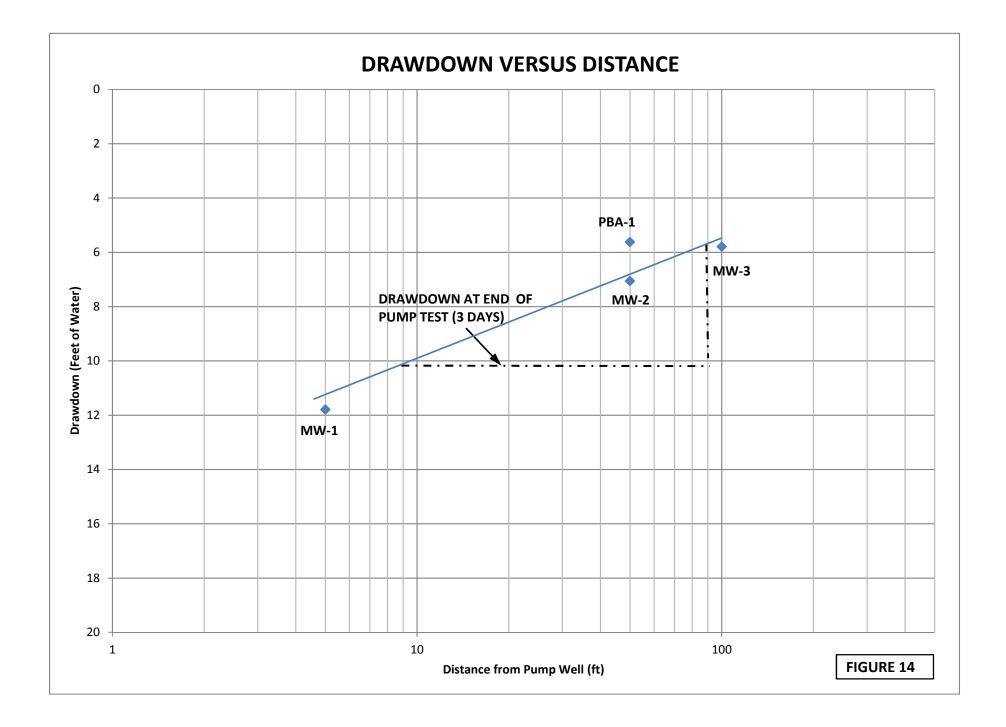


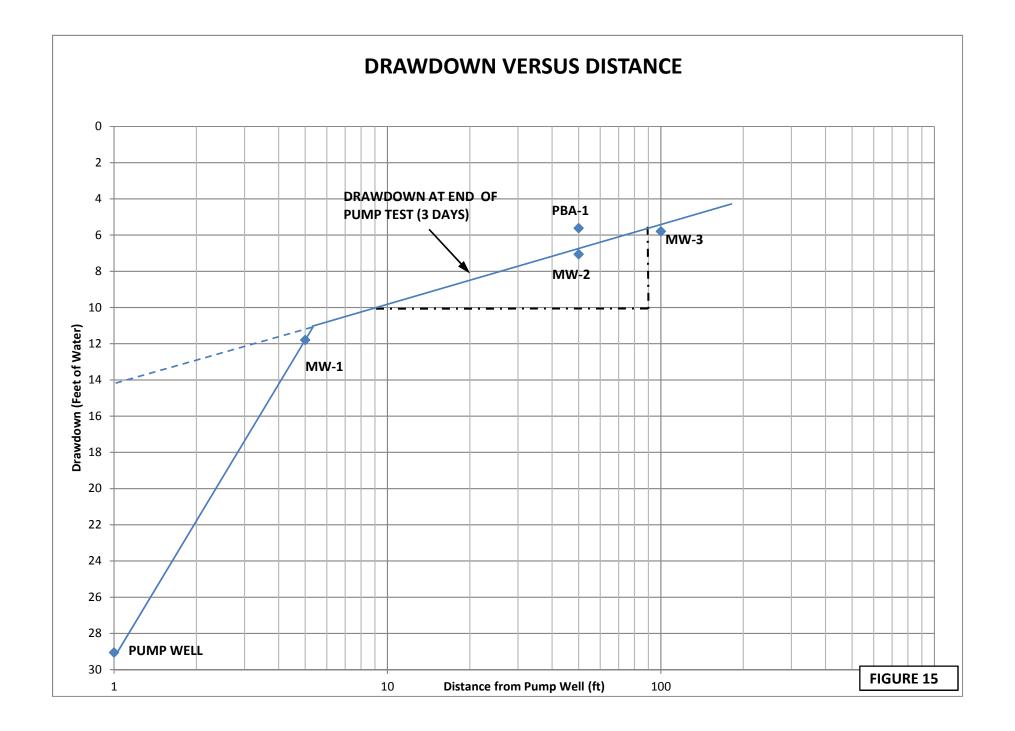












APPENDIX A

LIMITATIONS

LIMITATIONS

A. Explorations

- 1. The analyses, conclusions and recommendations submitted in this report are based in part upon the data obtained from subsurface explorations, groundwater monitoring wells, pump well and pump tests performance. The nature and extent of variations between and beyond these explorations and wells may not become evident until construction. If variations then appear evident, it will be necessary to reevaluate the recommendations of this report.
- 2. The generalized soil profiles described in the text and shown on the figures are intended to convey trends in subsurface conditions. The boundaries between strata are approximate and idealized and have been developed by interpretations of widely spaced explorations and samples; actual soil transitions are probably more erratic. For specific information, refer to the boring logs.
- 3. Groundwater level readings have been made in the borings, monitor wells and pump well at times and under conditions stated on the logs and data sheets. These data have been reviewed and interpretations have been made in the text of this report; however, it must be noted that fluctuations in the level of the groundwater may occur due to a variety of reasons including: variations in rainfall, temperature, tide, season and other factors occurring since the time measurements were made.

B. Review

1. In the event that any changes in the nature, design, or location of the proposed structures are planned, the conclusions and recommendations contained in this report shall not be considered valid unless the changes are reviewed and conclusions of this report are modified or verified in writing by Paul B. Aldinger & Associates, Inc. It is recommended that this firm be provided the opportunity for a general review of final design and specifications, in order that groundwater and foundation recommendations may be properly interpreted and implemented in the design and specifications.

C. Construction

1. It is recommended that this firm be retained to provide soil engineering services during construction of the support of excavation, dewatering, excavation and foundation phases of the work. This is to observe compliance with the design concepts, specifications, report conclusions and recommendations, and to allow design changes in the event that subsurface conditions differ from those anticipated prior to the start of construction.

D. Use of Report

- 1. This report has been prepared for the exclusive use of BETA Group, Inc. for specific application to the proposed Pump Station and Stream Crossing in Taunton, Massachusetts in accordance with generally accepted soil and foundation engineering practices. No warranty, express or implied, is made.
- 2. This report may contain comparative cost estimates for the purpose of evaluating alternative construction schemes. These estimates may also involve approximate quantity evaluations. It should be noted that quantity estimates may not be accurate enough for construction bids. Since Paul B. Aldinger & Associates, Inc. has no control over labor and materials cost and design, the estimates of construction costs have been made on the basis of experience. We cannot guarantee the accuracy of cost estimates as compared to contractors' bids for construction costs.

APPENDIX B

- Boring Logs PBA-1 and PBA-2,
- Grainsize Analysis, Pump Test Screen Stratum: Soil sample from boring PBA-1, Glacial Outwash 2 Stratum, Sample depth 49 to 56 feet below ground surface.

Client N	lame	New Hampshire Boring, Inc. Sheet 1 of 2 Boring No. PBA-1					-1					
P. B. Aldinger & Associates		215 W. Chestnut Street Brockton, MA 02301 NEBC JOB					36951 PBA J	lob No. 1700	6			
City/Tow	n: Taunton, I	Ma.			BIOC		02301	PROJI	ECT NAME:	: Pump Statio	n & Water Cr	ossing
Location	: Pump Station,	North					Date & Time S	Started	Date & Tin	ne Completed	Total Hou	rs Worked
Groundw	vater Depth (Feet)	: 8.0)' E.O.I	B. 7.	.2' on 3	/3/17	2/27/201	7	2/2	8/2017		
DRILLEF	R: Norman Stude	lard					HELPER:					
Ground I	Elevation: +11.	5'		Inspec	tor's Na	ame:	Bryan Deely		Inspector's	Company:	P.B. Aldinge	er
Sample	Depth Range	Blow	Counts	s per 6	Inches	Recovery		Field	d Descript	tion		Strata
Number	(Feet)	0-6	6-12	12-18	18-24	(inches)						Changes
							ASPHALT					3"
S-1	6" - 2'6"	44	33	28	47	12"	Medium dense, brow		E TO COAR	SE SAND, littl	e gravel,	
							little inorganic silt (Fi					
S-2	4'- 6'	26	13	13	8	6"	Medium dense, brov	vn INOI	RGANIC SII	T, little fine to	coarse	FILL
							sand (Fill).					
S-3	9' - 11'	18	7	3	3	5"	Loose, gray INORG	ANIC S	ILI, little fin	e to coarse sa	nd (Fill).	
A (
S-4	14' - 16'	7	3	2	4/5"	18"	Loose, gray INORG/ at 16 (Fill)'.	ANIC S	IL I, little fin	e to coarse sa	nd, WOOD	
							L <u></u>					16'
S-5	19' - 19'3"	10	0/3"			3"	WOOD.					20'
_							Madium danaa amay					
S-6	24' - 26'	26	13	16	26	19"	Medium dense, gray	VARV	ED INORG/	ANIC SILT.		
_							Madium danaa amay			-		
S-7	29' - 31'	11	13	18	26	14"	Medium dense, gray					
							Medium dense, brov silt.			JIVI SAND, ITAC	e morganic	
_												
S-8	34' - 36'	8	7	7	6	24"	Medium dense, gray	, VARV	ED INORG	ANIC SILT.		SILT
							Madium danaa muu			-		
S-9	39' - 41'	10	19	17	13	11"	Medium dense, gray INORGANIC SILT.					
												40'
S-10	44' - 46'	29	27	26	18	12"	Wet, very dense, gra inorganic silt, trace g	-		(SE SAND, tra	ce	
											ener (el	FINE TO
S-11	49' - 51	27	9	8	7	12"	Medium dense, gray trace inorganic silt.	, FINE	TO COARS	SE SAND, little	gravei,	COARSE
												SAND
Remark	ks: E.O.B. = I	End of	boring	g								
				<u>,</u>					Casi	ng Used: HW	and NW	
					sistanc	e (N) Guid				•		
	hesionless Soils (,			sive Soils (Silts, Clay			ng Size: 4"	and 3"	
	ve Density Per y Loose		on Resis	stance		Consistency Very Soft	y Penetration 0 -			mer Weight	300lbs.	
	.00se		- 10		Soft 2 - 4				200100.			
	um Dense		- 30		Ν	/ledium Stil					24"	
)ense v Dense		- 50			Stiff						
Very Dense Over 50					Very Stiff Hard	- Over			Hammer Weight 140lbs. Drill Rig Type: CME 75 Truck Mount			
N = Sı	um of Second and T	hird 6"	Blow Co	ounts	S		of Descriptions: and = 3					

Client Name						pshire Bo Chestnu	•		Sheet	2 of 2	Boring I	No. PB	A-1	
P. B. A	ldinger & Asso	ciates		•	-	ton, MA			NEBC	JOB No: 3	OB No: 36951 PBA Job No. 170			
City/Tow	n: Taunton,	Ma.							PROJI	ECT NAME	: Pump Statio	n & Water (Crossing	
Location	: Pump Station,	North						Date & Time S	Started	Date & Tir	me Completed	Total Hou	urs Worked	
Groundw	ater Depth (Fee	t): 8.0	' E.O.B.	7.2' c	on 3/3/1	7		2/27/201	7	2/2	8/2017			
DRILLEF	R: Norman Stud	dard						HELPER:		•		•		
Ground I	Elevation: +11	.5'		Inspec	tor's Na	ame:		Bryan Deely		Inspector's	Company:	P.B. Alding	ger	
Sample	Depth Range	Blow	Counts	per 6 l	nches	Recovery					· · ·		Strata	
Number	(Feet)	0-6	6-12	12-18	18-24	(inches)			Field	Descript	ion		Changes	
S-12	54' - 56	17	10	11	14	7"	Mediu	m dense, gray	FINE	TO COARS	E SAND, trace	e inorganic	FINE TO	
							silt.						COARSE SAND	
S-13	59' - 61'	33	23	38	26	12"	Very o	lense, gray FI	NE TO	COARSE S	AND, some gr	avel, trace	SAND	
							inorga	inic silt.					63'	
S-14	64'- 66'	21	28	39	30	17"	Verv o	lense, gray FI		ID.			F. SAND	
011	01 00	21	20	00	00		ſ						68'	
S-15	69' - 71'	42	68	56	51	12"	Verv o	lense, gray FI		COARSE S	AND AND GR	AVEL.	TILL	
0-10	09-71	42	00	50	51	12	-	norganic silt (0				,	72'	
S-16	74'	100/0'					Proba	ble Bedrock					BEDROCH	
3-10	74	100/0	1										74'	
							Bottor	n of Exploratio	n = 74'				14	
							Dolloi		11 - 74					
							-							
							Install		11	terine Mall	to 15 feet door	th.		
							Install	ed Groundwate	er ivioni	toring vveil	to 45 foot dep	IN		
								ized Groundwa e, March 3, 20		ding 7.21 fe	et below pave	ment		
							Sunac	c, March 0, 20	, , ,					
]							
		1					1							
		<u> </u>					1						<u> </u>	
Remark	(s: <u>E.O.B.</u> =	End of	Boring	8		·						, ,		
			Donet	tion D-	oioto					Casi	ng Used: HW	and NW		
Col	nesionless Soils				อเอเสทต	e (N) Guide Cohe		oils (Silts, Clays	s)	Casi	ng Size: 4"	and 3"		
		enetratio			(Consistency	у	Penetration			5			
-	y Loose	-) - 4			Very Soft		0 -	_	Ham	mer Weight	300lbs.		
	oose ım Dense		- 10) - 30		N	Soft /ledium Stit	ff	2 - 4 -		Colit	Spoon Size:	1 3/8" ID X	(24"	
	lin Dense		- 30 - 50			Stiff	11	4 - 8 -	-	Spill	opoon size.		~ 27	
	/ Dense		/er 50			Very Stiff		15 -	30		mer Weight	140lbs.		
					Hard			Over			Drill Rig Type: CME 75 Truck Mount			
N = Si	um of Second and	Third 6"	Blow Co	unts	Se	econd Entry	of Desc	riptions: and = 3	5-50%, s	some = 20-3	5%, little 10-20%	6, trace = 109	% or less	

Client N	lame				-		oring, Inc.	Sheet	1 of 2	Boring N	lo. PBA	-2
P. B. A	ldinger & Assoc	iates				Chestnu ton, MA		NEBC JOB No: 36951 PBA Job No. 1700				
City/Tow	n: Taunton,	Ma.	•					PROJ	ECT NAME:	Pump Statio	n & Water Cr	ossing
Location	: Pump Station,	South					Date & Time S	Started	Date & Tim	e Completed	Total Hou	rs Worked
Groundw	ater Depth (Feet): 8.0)' E.O.I	B.			2/28/202	17	3/1/	2017		
DRILLEF	R: Norman Stude	dard					HELPER:					
Ground I	Elevation: +11	.5'		Inspec	tor's Na	ame:	Bryan Deely		Inspector's	Company:	P.B. Aldinge	r
Sample	Depth Range	Blow		s per 6 l		Recovery		Fiol	d Descripti	ion		Strata
Number	(Feet)	0-6	6-12	12-18	18-24	(inches)			u Descripti			Changes
							ASPHALT					3"
S-1	6" - 2'6"	8	14	17	12	15"	Dense, brown FINE	TO CO	ARSE SAN	D, little gravel	trace	
							inorganic silt, (Fill.)					
S-2	4'- 6'	18	7	7	9	17"	Medium dense, gray	/ FINE	TO COARSE	SAND, som	e inorganic	
							silt, little gravel.					FILL
S-3	9' - 11'	8	8	8	11	15"	Medium dense, brow	wn FINE	E TO MEDIU	M SAND, trad	ce inorganic	
							silt, (Fill.)					
S-4	14' - 16'	18	12	13	11	20"	Medium dense, mot	tled, ora	ange-gray SI	LT (Fill).		15'
							Medium dense, gray	/ FINE	TO COARSE	SAND, little	silt.	17'
S-5	19' - 21'	13	8	7	11	3"	Medium dense, gray	/ INOR	GANIC SILT.	•		••
00	10 21	10	Ŭ	, ,		0						
S-6	24' - 26'	16	12	8	9	19"	Medium dense, gray	/. varve	d INORGAN	IC SILT.		
3-0	24 - 20	10	12	0	9	19		,,				SILT
S-7	29' - 31'	7	7	8	9	21"	Wet, medium dense	liaht h	rown varver		SILT	SILI
5-7	29 - 31	1	1	0	9	21		, ngin b			JOILT.	
0.0	0.41 0.01		0	_	_	0.01	Wet, medium dense	light h				
S-8	34' - 36'	9	8	5	7	23"	wet, medium dense	, iigin b			JULI.	
							Mot modium donoo	arov F				38.5'
S-9	39' - 41'	31	17	9	12	8	Wet, medium dense GRAVEL, some inor			ARSE SAND	AND	
-								•				
S-10	44' - 46'	15	7	8	9		Wet, medium dense inorganic silt.	, gray F	INE TO CO	ARSE SAND	trace	FINE TO
								_				COARSE
S-11	49' - 51'	12	12	15	15	18"	Wet, medium dense trace inorganic silt.	, gray F	INE TO CO	ARSE SAND,	little gravel,	SAND
							trace morganic sit.					
Remark	(S. F.O.	B = F	nd of b	oring								
Condit		<u> L</u>		501115				·	Casin	g Used: HW	and NW	
		F	Penetra	tion Re	sistance	e (N) Guid	2					
	nesionless Soils (Sands,	Grave	ls)			sive S <mark>oils (Silts, Clay</mark>			ig Size: 4"	and 3"	
	,		n Resis	stance	C	Consistenc					2001	
	y Loose oose		- 4 - 10			Very Soft Soft	0 - 2 -		Hamr	ner Weight	300lbs.	
	im Dense		- 30		N	ledium Stit			Split \$	Spoon Size:	1 3/8" ID X 2	24"
D	ense		- 50			Stiff	8 -					
1/0-	/ Dense	Ov	er 50		1	Very Stiff	15 -	- 30	Hamr	ner Weight	140lbs.	
very	Dense	•••	0. 00			Hard	Ove			Rig Type:	CME 75 Tru	ok Maxint

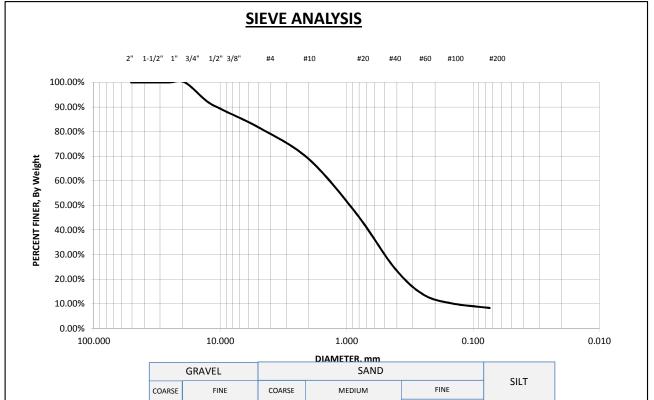
Client N		. ,			-	pshire Bo Chestnu	-		Sheet	2 of 2	Boring	No. PBA	-2	
	Idinger & Asso					ton, MA					6951 PBA			
City/Tow										T	Pump Statio			
	: Pump Station,							Date & Time S			e Completed	Total Hou	rs Worked	
	vater Depth (Fee	-	D' E.O.E	3.				2/28/201	17	3/1/	2017			
DRILLE	R: Norman Stud	dard		r				HELPER:		1				
Ground	Elevation: +11	-			tor's Na	ame:		Bryan Deely		Inspector's	Company:	P.B. Aldinge	er	
Sample Number	Depth Range (Feet)	Blow 0-6	Counts 6-12	s per 6 12-18		Recovery (inches)			Field	d Descripti	on		Strata Changes	
S-12	54' - 56	5	6	11	12	18"		ım dense, gray inorganic silt.	y FINE ⁻	TO COARSE	SAND, trace	e gravel,	FINE TO COARSE	
S-13	59' - 61'	22	15	12	15	24"	Mediu trace	ım dense, gray silt.	FINE	TO COARSE	SAND, trace	e gravel,	SAND	
S-14	64' - 65'5"	19	47	10	0/5"	14"	Very	dense, gray Fl	NE TO	MEDIUM SA	JM SAND, trace inorganic silt.			
S-15	69' - 71'	122	39	32	45	15"		dense, gray Fl anic silt (Glacia		COARSE SA	AND AND GR	AVEL, little	67' TILL 71'	
S-16	74'	100/0'	ı '				Proba	ble BEDROCH	۲				BEDROCK	
0.0			[74'	
							Botto	m of Exploratio	on = 74'					
							-							
							1							
Remar	ks: <u>E.O.B.</u> =	End of	borin	g	·	·	·			Casin	g Used: HW	/ and NW		
		F	Penetra	tion Re	sistance	e (N) Guid					-			
	hesionless Soils							oils (Silts, Clay			g Size: 4"	and 3"		
		netratio	on Resis	stance		Consistenc	-	Penetration 0 -			nor Woight	300lba		
	y Loose .oose	-	- 4			Very Soft Soft		0 - 2 -		Hamr	ner Weight	300lbs.		
	um Dense		- 30		N	ledium Sti	ff	_	- 8	Split S	Spoon Size:	1 3/8" ID X	24"	
	Dense		- 50			Stiff		-	8 - 15					
	Very Dense Over 50				Hard (15 - Over	r 30	Hammer Weight 140lbs. Drill Rig Type: CME 75 Truck Mount , some = 20-35%, little 10-20%, trace = 10% or less				
N = S	um of Second and	Third 6"	Blow Co	ounts	S	econd Entry	/ of Des	scriptions: and =	35-50%	, some = 20-3	5%, little 10-20	0%, trace = $10%$	% or less	

SIEVE ANALYSIS

DESCRIPTION:	Fine to coarse SAND, little Gravel, trace Silt	PROJ:	Pump Station & Water Crossing
		LOCATION:	Taunton, MA
		JOB #:	17006
Sample Location:	Taunton, MA	DATE:	6/9/2017
		CONTAINER #:	47
USCS:	SW-SM	CONT.+ WET SOIL:	636.44
TEST BORING NO.:	PBA-1	CONT.+ DRY SOIL:	585.97
DEPTH:	49'-56'	WGT WATER:	50.47
SAMPLE #:	S-11,S-12	CONT WGT:	177.51
WASH SIEVE	yes	DRY SOIL:	408.46
		% MOIST:	12.36%

SIEVE	OPENING	WEIGHT	ACCUM.	PERCENT	TOTAL %	PROJECT
	(MM)	RETAINED	RETAINED	RETAINED	FINER/WGT	SPEC.
3"	76.2	0.00	0.00	0.00%	100.00%	
2"	50.800	0.00	0.00	0.00%	100.00%	
1 1/2"	37.500	0.00	0.00	0.00%	100.00%	
1"	25.400	0.00	0.00	0.00%	100.00%	
3/4"	19.100	0.00	0.00	0.00%	100.00%	
1/2"	12.700	31.66	31.66	7.75%	92.25%	
3/8"	9.525	14.25	45.91	11.24%	88.76%	
4	4.750	31.14	77.05	18.86%	81.14%	
10	2.000	50.05	127.10	31.12%	68.88%	
20	0.840	90.57	217.67	53.29%	46.71%	
40	0.420	90.09	307.76	75.35%	24.65%	
60	0.250	43.99	351.75	86.12%	13.88%	
100	0.149	15.03	366.78	89.80%	10.20%	
200	0.074	7.83	374.61	91.71%	8.29%	
Pan	0.000	33.85	408.46	100.00%	0.00%	
OTAL DRY WT.			408.46			

	% GRAVEL	% SAND	% SILT & CLAY
TOTAL	18.9%	72.8%	8.3%
COARSE	0.0%	12.3%	
MEDIUM		44.2%	
FINE	18.9%	16.4%	



PBA-1 (S-11, S-12)

APPENDIX C

- J. Russell Water Well Inc. Information Package:
- Step and Pump Tests, Pump Well Summary Data,
- Pump Well Installation Log,
- Pump Well Submersible Pump Performance Curves,
- Step and Pump Tests, Pump Well: Pump Rate, Groundwater Level Monitoring Data, Time.

J. RUSSELL WATER WELL INC.

P.O. Box 1025 Hope Valley, RI 02832 (401) 539-2739 Well Drilling Complete Water Systems Water Testing Water Treatment

72 HOUR PUMP TEST

WEST WATER STREET TAUNTON PUMPING STATION

A 72-hour pump test was conducted on an 8-inch diameter screened gravel developed well at the West Water Street Pumping Station in Taunton Massachusetts. This well is 60 ft. deep with 10 ft. of 50 slot stainless steel well screen.

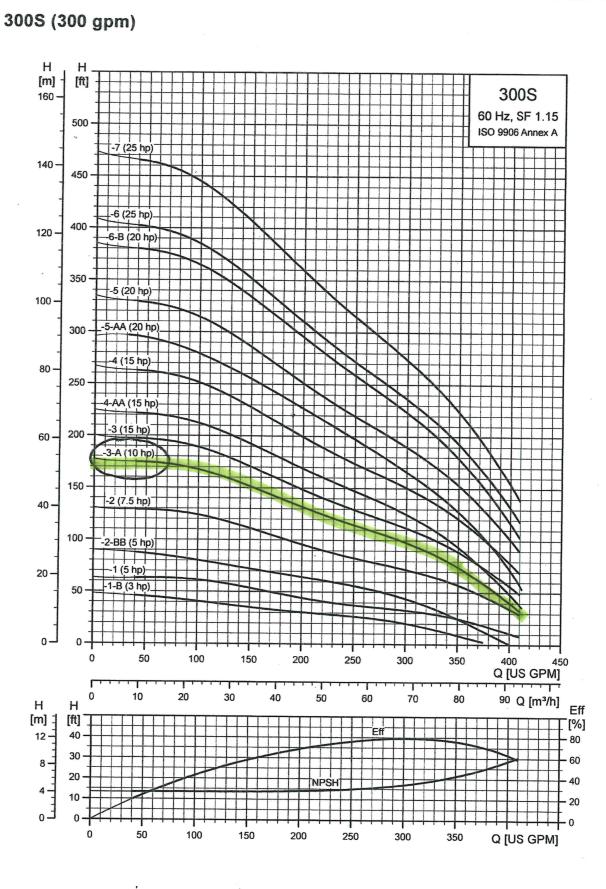
A Grundfos model 300S100-3A submersible turbine pump was installed for this test. This threestage turbine can pump a maximum of 400 gpm against 50 ft. of head. The pump intake was set at 43 ft. below land surface. A stilling tube was also installed to allow unobstructed hand measurements with a Solonist electric tape measure. The water was discharged through approximately 45 ft. of PVC pipe to an underground chamber near the pumping station building. Discharge was measured with an in-line digital flow meter installed about 25 ft. from the well.

On 3/19/18 a step test was performed to determine a sustainable pumping rate for this threeday test. The static water level was 7.16 ft below the measuring point. (The M.P. was the top of the well, 1.90 ft above land surface).

The first step was at 100 gpm, which produced 15.79 ft. of drawdown. The second step was at 150 gpm, which produced 19.94 ft. of drawdown and the third step was at 200 gpm which produced 26.84 ft. of drawdown, (a pumping W.L. of 34.00 ft.). This left a safe reserve of 10.9 ft. of additional available drawdown above the pump intake. Aldinger and Associates determined that this was a safe rate that would sufficiently produce an aquifer response.

The well was allowed to recover to within 0.34 ft. of static before starting the 3-day test. At 12:45 on 3/19/18 the pump test began. A constant rate of 200 gpm was maintained until the end of the test at 13:05 on 3/22/18. A total of 30.39 ft. of drawdown was measured, (pumping W.L. of 37.55 ft.). The well recovered to within 1.8 ft. of static within 30 minutes after shutting the pump off. The following day all equipment was removed.

Curve charts and technical data



54 GRUNDFOS·X

TAUNTON WEST WATER ST. Well Drilling and Pump Installation P.O. Box 1025 Hope Valley R.I. 02832 J. RUSSELL WATER WELL INC.

PUMPIUS STATION

PUMPING TEST DATA

Well No. 8"well

mP= T.O.C

Sheet / of 3

Obser-	Inato	Imimo	Imimo	P-0000	L Mana	74.5 m m m m				
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			pump on	W.L. Rec. 1.90 A Above	Held	Wet	Depth			P RATE 9PM
				1-90 At Above			below		PBA-1	Deal
			(min)	LS (ft)		l	MP			1254
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J. RUSSELL WATER WELL INC. Well Drilling and Pump Installation 5* P.O. Box 1025 Hope Valley R.I. 02832

Pumping STATION

TAUNTON WEST WATER ST

PUMPING TEST DATA

No. $\underline{\beta}^{4}$ well M^{9} -To.C. Sheet $\underline{\partial}$ of Dbser- ver Date Time since pump on (min) $E^{-TapeAS}$ (ft) Tape Measurement held $U/gllpelatic$					PUBPIN	G TES	r daya	L			
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$\begin{array}{ c c c c c c c c c c c c c c c c c c c$				pump on	W.L. Rec. 1,90 FT Above	Held	Wet	Depth	an sin	8	RATE
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וחיייייי	Casing Blows Per Ft.	San No.	nple Depths From-To	Materiai	Strata Change	SOIL IDENTIFICATIO Remarks include color, gradat soil, etc. Proportions used: Little 10-20%; some 20-35% ar	tion, type of Trace 0-10%;	Drilling Ti Water Los Sample Tyn
0				DRIII WS - A RELIET DRUINS - M	water 748ie B	Iditele 10-20%; some 20-35% ar Asphalt Then fill-3 GRAVEL, BOULDERS, PIECES BROWN 0-5 FILL, Then FINE SAN SILT BROWN 5-10 Fine SAND WITH SILT Chemical SMELL AT WATCH BROWN 10-15 FINE SILTY SAND TO 16 17-20 GRAY SILT/CLAY GRAY 15-20 MUD DRILLING-SCREENED VUITH LOSS OF FINE PARTICLE 20-23 NO RECOVERY-PROBAD 23-25 CDARSE SAND W GRANCH 20-25 D COARSE SAND, SOME VC SAND, LIT	SAMIS, of WOOD ID WITH R TABLE FT; Then SAMPLES Sizes Le Sizt AL GRAVE(L. J. BROWN	Water Level
(DUM - 2000	-	LT. BROWN 25-30 SAME W/SOME GRAVE GRAVEJ 30-35 SAME ALSO WITH LA Cobbles - ROUSH DREILING 35-40 VC SAND AND PEDDLE GRAVE	₹ <u>5.0</u>	
						5524 W/Blue 40- 47		1-9-18

CATION Pund STATION		Drilling and Pump Installation BORING FO	REMAN RRosser
Sample Depths d rog.	Strata Change	SOIL IDENTIFICATION Remarks include color, gradation, type of soil, etc. Proportions used: Trace 0-10%;	Drilling Ti Water Los Sample Typ
		Set 8 Wich <asing 42="" drove<br="" ft,="" then="" to="">RecAsing TO 62 FT VC SAND + PEBBE BRAVEL VC SAND + 984NULAR GRAVEL</asing>	Water Level
0 Windsheep Samples		ANGULAR <u>1314CK</u> 50-55 55-57/1L SAND + GRANJUR GRANNE, HAD TO DRILLOUT SMALL COUDLES 57-62 COARSE SAND 1 SOME VC SAND 55-62 LITTLE MED SAND 134ACH	
		SS-62 GRANULAR GRAVEL; Some Debble GRAVEL LITTLE COARSE SAND 62-65 BLACK ** ** ** ** ** ** ** ** ** ** ** ** **	
		20-47 SAMPLES by MUD DRITTING, SAMPLES WERE SCREENED AND WAShed with Loss of Fine PARTICLE SIZES 47-65 SAMPLES WERE WASLED TO The SURPACE WITH WATER	
		- WOOD Feberes AND LEAF PARTIcles in the samples were Recirculated from the mous Pit.	1-10-18

J. RUSSELL WATER WELL INC.

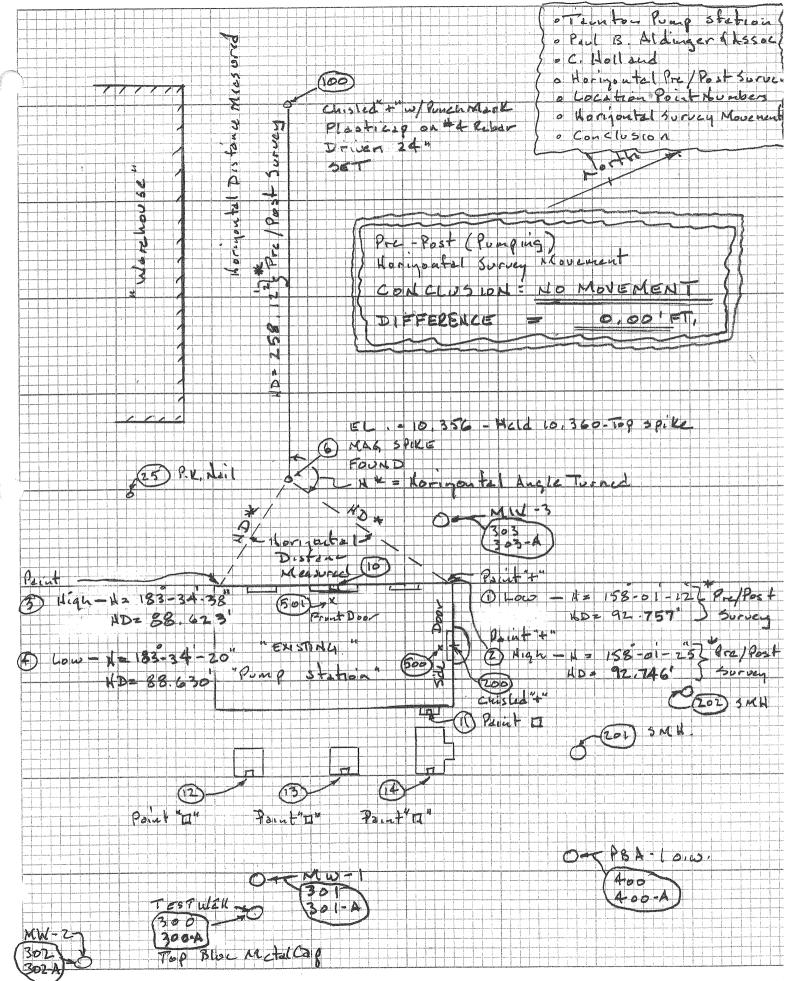
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TEST HOLE SUMMARY

Property Owne Owner's Addre Purpose of he Altitude of		8"-1. TAUNTON MA Date Started 1-9-18 Date Completed 1-11-18 Lat. Long.
	FINISH WELL Diameter <u>8</u> in. Screen Slot # <u>Sofrom <u>50</u> (ft) to <u>60</u> (ft) # <u>from (ft) to (ft)</u> Water level below LSD <u>3.300</u> (ft) at <u>14320 1-11-20</u>Hr/Date From LSD (ft) <u>Aloo</u> to top of casing <u>50</u> to top of riser <u>50</u> to top of screen <u>356</u> t. length of screen <u>70</u> ft. length of screen <u>70</u> ft. riser + screen <u>60</u> to bottom of screen DATE CASING PULLED </u>	Pumped from to at gr in. vac. Method 2/ FIELD WATER QUALITY DATA Sample taken (Hr/Data after pumping gpm for H Temp. C° D.0 mg S. Cond. unho Alk. pH LABORATORY WATER QUALITY DATA (mg/1) Fe C1 Mn N03 REMARKS (Sketch map on reverse side) ScReen Development was Dave using com pressed Air 300 GPM estimated Yield DRiller: Sim Veria Maspetar: S. Russell
	<pre>1/ D, diaphragm; S, surge block; T, turbin 2/ C, centrifugal; D, diaphragm; T, turbine</pre>	

APPENDIX D

- Surveyor's Sketch, Existing Pump Station Vertical Movement Monitoring Point Locations, and Monitoring Point Spreadsheet Data,
- Main Lift Pumping Station, Taunton, MA, "Vertical Control (Locations)," Figure 1, BETA Group Inc.



Rite in the Rain-

No. 1110 1/10" grid

		Taunton Main Lift Pumping Sta	ation and St	ream Crossin	g					• Paul B. Aldinger and	Associates, Inc.		
		Taunton,	, MA							 Survey Dates: Fri. Fe 	b 02; Mon. Feb 05; We	ed. Feb 28; and Fri. Mar 2	.3, 2018
		Pre - Post Pumping Flo	w Test Mon	itoring						• Survey Onsite By: Ch	arles Holland, Bryan D	eely, David Nacci or Mik	e
		Vertical Survey of Structu	ure/Point M	ovement						• Spreadsheet No. 1 o	f 1		
Location	Pre-Survey (Pumping)	Pre-Survey (Pumping FT)		y (Pumping)	Pre-Survey				ey (Pumping)	Pre-Post (Pumping) S		Pre-Post (Pumping)	Bench Marks
Point	Fri. !	Feb 02 2018	Mon. Feb Elev. + (N	b 05 2018 NAVD88)	Wed. Feb Elev. + (N				ar 23 2018 (NAVD88)	Variation ((+) = upw Elev. + (I	ard, (-) = downward) NAVD88)	Survey Movement Determination	on Site Plan Set Elev. + (NAVD88)
No.	Found	Set	Found	Set	Found	Set		Found	Set	Difference (foot)	Difference (Inches)	Conclusion	Found
1		Paint "+" Cross		n/a		13.145			13.145	0	0	0"	
2		Paint "+" Cross	<u> </u> '	17.190		17.195			17.200	0.005' + to 0.010' +	1/16" + to 1/8" +	0"	
3		Paint "+" Cross		17.160		17.160			17.160	0	0	0"	
4		Paint "+" Cross	['	n/a		13.160			13.160	0	0	0"	
6	Mag Spike/Punch Mark (Bench Mark Held)	V	10.360		10.360			10.360		0	0	0"	10.356
10		Paint "[]" Sq.	 '	12.965		12.965			12.970 - 12.965	0.005'+ to 0'	1/16" + to 0"	0"	
11		Paint "[]" Sq.	['	12.985		12.990			12.990	0.005' +	1/16" +	0"	
12		Paint "[]" Sq.	í	12.610		12.620			12.610	0.010' + to 0'	1/8" + to 0"	0"	
13		Paint "[]" Sq.	Į′	12.605		12.610			12.600	0.005' + to 0.010' -	1/16" + to 1/8" -	0"	
14		Paint "[]" Sq.	 '	12.645		12.655	ø		12.645	0.010' + to 0'	1/8" + to 0"	0"	
25	PK Nail in Bit Pavement		n/a		10.065		, 2018	10.060		0.005' -	1/16" -	0"	10.030
200	Chisled "+" CL Step Metal Edge		12.960		12.960) - 22,	12.960		0	0"	0"	13.000
201	SMH Rim	P	n/a		11.420		19 Aar	11.415		0.005' -	1/16" -	0"	11.40 +/-
202	SMH Rim	P	n/a		11.870		Testing: N	11.865		0.005' -	1/16" -	0"	11.97 - 12.18 +/-
300		Test Well w/ Blue Metal Cap Top @ Arrow Marker	Í	n/a		n/a	Test		13.385				
300-A		Test Well w/ Blue Cap @ Ground	 '	n/a		n/a	Pump		11.385		 		
301		MW-1 Top 1" PVC		n/a		n/a	Ā		13.230		 		
301-A		MW-1 Ground	, ['	n/a		n/a			11.385				
302		MW-2 Top 1" PVC	ſ'	n/a		n/a			10.855		ļ!		
302-A		MW-2 Ground	Į′	n/a		n/a			7.720				
303		MW-3 Top 1" PVC	'	n/a		n/a			11.235				
303-A		MW-3 Ground	ļ'	n/a		n/a			10.415				
400		PBA-1 Test Boring Top 1" PVC @ Arrow Marker	j′	n/a		n/a			11.095				
400-A		PBA-1 Test Boring Casing/Grade	′	n/a		n/a			11.290				
500	1st Floor Conc., 6"-12" Inside <u>SIDE</u> Door		n/a		13.030			13.030		0'	0"	0"	13.070
501	1st Floor Conc., 3"-6" Inside <u>FRONT</u> Door		n/a		13.085			13.080		0.005' -	1/16" -	0"	12.970

